

Antimicrobial activity analysis and QSAR studies of p-coumaric Acid derivatives using physicochemical parameters

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ABSTRACT

A Quantative-Structure-Activity Relationship (QSAR) study is performed on set of 36 p-coumaric Acid derivatives and number of highly descriptive and predictive QSAR models for these compounds were obtained by Using physicochemical parameters using stepwise-multiple linear regressions methods.. Model validation is performed by incorporating training and test sets approach and calculating R^2 which is equal to 0.5979 and also Regression analysis data has indicated that activity can be best modeled in multi-parametric regression.

Keywords: p-coumaric Acid derivatives, QSAR, Molar Volume, Molar Refractivity, Parachore, Density, Refractive Index, Surface Tension, Polarizability

INTRODUCTION:

Development of new and different antimicrobial drugs is an important objective and much of research program efforts are directed towards the design of new agents, the reason being that the usage of most antimicrobial agents is limited, not only by the rapidly developing drug resistance, but also by unsatisfactory status of present treatment of bacterial and fungal infections and drug side effects [1-3]. Some substituted anilides, which very recently appeared in literature, have received considerable attention due to their wide range of biological activities viz. antibacterial, antifungal, anticonvulsant, anaesthetic, antiproliferative, antiplaque, antiplatelet-aggregation, antioxidant and potassium channel activating potentials [4-13].

QSAR analysis is a widely used statistical methods to describe the relationship between chemical structure and biological activities of a series of analogs quantitatively [14]. In view of the above and in continuation to our work on QSAR studies in describing the biological activity [15-22], in the present study we report the QSAR studies of p-coumaric acid derivatives using physicochemical parameters.

Experimental Details

For QSAR study MIC values in $\mu\text{g/ml}$ were transformed into pMIC values.(i.e. $-\log \text{MIC}$ in $\mu\text{g/ml}$) which are reported in table A-I

Parameters used

We have used following physicochemical parameters for modeling of pMIC_{ab} and pMIC_{am} of various pCoumaric acid derivatives which were calculated by using ACD labs software ChemsSketch[14].

(1)Molecular volume (MV)

$$MV = \frac{MW}{d}$$

(2) Molar refractivity (MR)

$$MR = \frac{n^2-1}{n^2+2} \cdot \frac{MW}{d}$$

(3) Parachor (P)

$$P_r = \left(\frac{MW}{d}\right) \gamma^{1/4}$$

(4) Density (d)

$$d = \frac{MW}{MV}$$

(5) Refractive Index(n)

$$n = \sqrt{\frac{2MR+MV}{MV-MR}}$$

(6) Surface tension (γ)

$$\gamma = \left(\frac{P_r}{MV}\right)^4$$

(7) Polarizability (α)

$$\text{Polarizability} = 0.3964308 \cdot MR$$

The compounds used in the present study with their values are reported in Table A-I, The values of various parameters obtained are reported in Table A-II.

Results and Discussion:

A) Modeling $pMIC_{ab}$ using Physicochemical parameters

A close look of table A-III reveals that

- 1) Out of Eight mono-parametric model, MW shows the highest regression value for the best model.
- 2) Out of ten bi-parametric model, MR and D together shows the highest regression value for the best model.
- 3) Out of ten tri-parametric model, MR, D and POL together shows the highest regression value for the best model.
- 4) Out of ten tetra-parametric model, MR, MV, IR and D together shows the highest regression value for the best model.

Mono-Parametric model

$$pMIC_{ab} = 0.0032(\pm 0.0005)MW + 0.4857 \quad (A-1)$$

N= 37, $R^2=0.5545$, $R^2A=0.5414$, Se= 0.0810, F=42.3120

When MR and D were taken together a bi-Parametric model has been obtained with improved statistics here R^2 comes out to be 0.5855.

Bi-Parametric model

$$pMIC_{ab} = 0.0092(\pm 0.0018)MR + 0.3638 (\pm 0.1593)D + 0.1743 \quad (A-2)$$

N=37, $R^2 = 0.5855$, $R^2A = 0.5604$, Se=0. 0793, F=23.3110

A tri-Parametric model has been obtained when MR, D and POL were taken together. In this model the R^2 shows significant improvement.

Tri-Parametric model

$$pMIC_{ab} = 1.5411(\pm 2.2556)MR + 0.3705(\pm 0.1609)D - 3.8647(\pm 5.6900)POL + 0.1586 \quad (A-3)$$

N=37, $R^2 = 0.5914$, $R^2A = 0.5531$, Se= 0.0799, F= 15.4410

A tetra-parametric model has been obtained when MR, MV, IR and D were taken together. In this model the R^2 shows significant improvement.

Tetra-Parametric model

However very small improvement is observed in a tetra-parametric model when MR, MV, IR and D have been taken as correlating parameter. This model has been found to be excellent for modeling activity of the compounds of the present study.

$$pMIC_{ab} = 0.0355(\pm 0.0277)MR - 0.0088(\pm 0.0093)MV - 2.6994(\pm 2.7679)IR + 0.4522(\pm 0.3316)D + 4.3574 \quad (A-4)$$

$$N=37, R^2 = 0.5979, R^2A = 0.5460, Se = 0.0806, F = 11.5230$$

Validation of model

The model has been validated by plotting a graph actual and predicted value of pMIC_{ab} activity as recorded in Table A-IV obtained from tetra- parametric model.

Cross- validated parameters

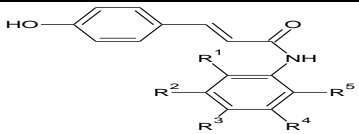
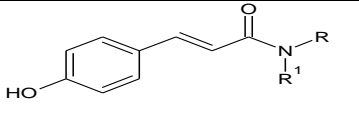
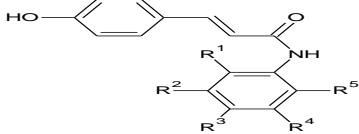
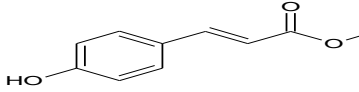
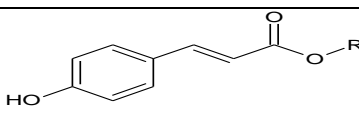
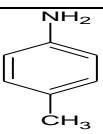
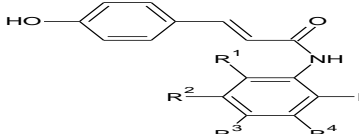
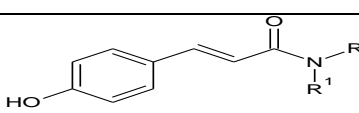
In this we observed the parameter with the high regression value which will obtained the best result.

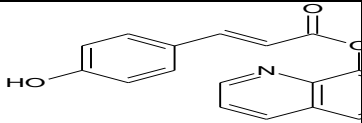
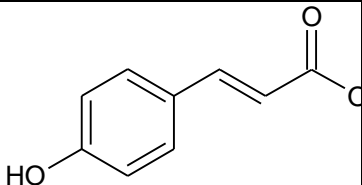

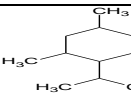
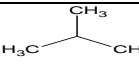
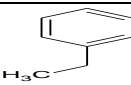
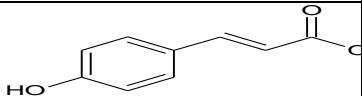
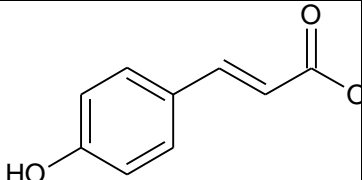
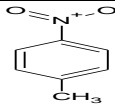
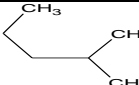
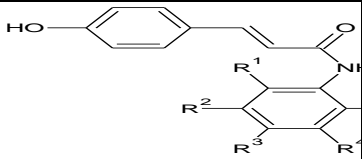
We have estimated pMIC_{ab} values using Model-29. The predictive power of best Model has been obtained by plotting graph between actual and predicted pMIC_{ab} values demonstrated in Fig. (a).

This clearly indicates that this is best model for estimating predicting pMIC_{ab} values of the compounds in the present study.

Table A-I Structural details of compounds under study.

S · N o ·	Parent structure	R	R 1	R 2	R 3	R 4			p M I C a b	p M I C a m
1			-	-	-	-			1 · 0 8	1 · 1 6
2		C ₆ H ₁ 3	-	-	-	-			1 · 4 0	1 · 3 6
3		-	-	-	-	-			1 · 3 5	1 · 3 5
4			-	-	-	-			1 · 2 3	1 · 2 7
5			-	-	-	-			1 · 5 3	1 · 3 9

6		H	C 1						1 . 6 1	1 . 5 3
7		O C H ₃	H						1 . 4 3	1 . 3 3
8		C ₂ H ₄ O H	C 2 H 4 O H						1 . 4 0	1 . 3 6
9		-	N O 2						1 . 3 6	1 . 4 2
10		C ₃ H ₇	-						1 . 2 2	1 . 1 6
11			-						1 . 3 1	1 . 3 1
12		-	H	C 1	C 1	H			1 . 3 9	1 . 3 3
13		-	H			N C 2			1 . 3 6	1 . 3 0
14		-	C H 3			H C 2			1 . 2 8	1 . 3 2
15		-	N H 2			H H H			1 . 3 1	1 . 2 5
16		C ₄ H ₉	C 4 H 9						1 . 2 4	1 . 2 2

17		-	-	-	-	-	-	1673	173
18			-	-	-	-	-	1197	117
19		C ₄ H ₉	-	-	-	-	-	1153	113
20			-	-	-	-	-	1384	144
21			-	-	-	-	-	1120	110
22			-	-	-	-	-	1219	119
23		C ₂ H ₅	-	-	-	-	-	1199	119
24		C H ₃	-	-	-	-	-	1155	115
25			-	-	-	-	-	1360	130
26			-	-	-	-	-	1171	112
27		-	H	N	H	H	-	1260	130
28		-	H	H	C	H	-	143	113

									4	4
29		C ₆ H ₅	C ₆ H ₅						160	146
30		-	-						146	124
31		-	C ₁₁	H ₁	N ₁	C ₂	H ₁		151	141
32		-	H ₁	C ₁	H ₁	H ₁			154	140
33		-	H ₁	H ₁	H ₁	H ₁			138	128
34		-	-						117	115
35		C ₃ H ₃	C ₃ H ₃						98	96
36		-	C ₃ H ₃		H ₁	C ₃ H ₃	H ₁		133	127

Table A-II Values of the calculated physicochemical parameters used in the present study

C o m p d . N a m e	M W	M R	M V	P C	I R	S T	D	P O L
1	2 4 0 . 2 5 3	7 0 . 3 0 0	1 9 4 . 3 0 0	5 2 2 . 3 0 0	1 . 6 4 3	5 2 . 1 0 0	1 . 2 3 6	2 7 . 8 7
2	2 4 7 . 3 3 2	7 5 . 4 4 0	2 3 3 . 8 0 0	5 9 6 . 9 0 0	1 . 5 5 8	4 2 . 4 0 0	1 . 0 5 7	2 9 . 9 0 0
3	2 8 1 . 3 0 6	8 2 . 6 0 0	2 2 1 . 9 0 0	6 1 2 . 5 0 0	1 . 6 6 6	5 7 . 9 0 0	1 . 2 6 7	3 2 . 7 4 0
4	2 6 7 . 2 7 9	7 7 . 2 4 0	2 1 0 . 6 0 0	5 7 8 . 7 0 0	1 . 6 5 4	5 6 . 9 0 0	1 . 2 6 8	3 0 . 6 2 0
5	2 6 8 . 2	7 5 . 3 3	2 0 3 . 9	5 7 2 . 9	1 . 6 6 0	6 2 . 3 0	1 . 3 1 5	2 9 . 8 6

	6 7	0	0 0	0 0		0		0
6	3 1 8 . 7 1 2	8 4 . 6 7 0	2 1 3 . 5 0 0	6 1 5 . 8 0 0	1 . 7 2 3	6 9 . 1 0 0	1 . 4 9 2	3 3 . 5 6 0
7	2 6 9 . 2 9 5	7 9 . 9 1 0	2 1 3 . 8 0 0	5 8 1 . 2 0 0	1 . 6 7 0	5 4 . 6 0 0	1 . 2 5 9	3 1 . 6 7 0
8	2 5 1 . 2 7 8	6 9 . 3 7 0	1 9 4 . 2 0 0	5 4 8 . 5 0 0	1 . 6 3 3	6 3 . 6 0 0	1 . 2 9 3	2 7 . 5 0 0
9	2 8 4 . 2 6 7	7 9 . 7 7 0	2 0 1 . 6 0 0	5 8 0 . 0 0 0	1 . 7 2 1	6 8 . 4 0 0	1 . 4 0 9	3 1 . 6 2 0
1 0	2 0 6 . 2 3 8	5 9 . 6 9 0	1 8 1 . 8 0 0	4 6 9 . 3 0 0	1 . 5 7 0	4 4 . 3 0 0	1 . 1 3 4	2 3 . 6 6 0
1 1	2 5 5 . 2 6 9	7 4 . 5 3 0	1 9 6 . 6 0 0	5 4 8 . 1 0 0	1 . 6 8 2	6 0 . 3 0 0	1 . 2 9 8	2 9 . 5 4 0

1 2	3 0 8 . 1 5 9	8 3 . 0 2 0	2 1 3 . 7 0 0 0	5 9 6 . 2 0 0	1 . 7 0 4	6 0 . 6 0 0	1 . 4 4 1	3 2 . 9 1 0
1 3	2 8 4 . 2 6 7	7 9 . 7 0	2 0 1 . 6 0 0	5 8 0 . 0 0 0	1 . 7 2 1	6 8 . 4 0 0	1 . 4 0 9	3 1 . 6 2 0
1 4	2 9 8 . 2 9 3	8 4 . 6 0 0	2 1 7 . 9 0 0	6 1 7 . 6 0 0	1 . 7 0 4	6 4 . 5 0 0	1 . 3 6 8	3 3 . 5 3 0
1 5	2 5 4 . 2 8 4	7 7 . 4 0 0	1 9 2 . 0 0 0	5 5 0 . 3 0 0	1 . 7 4 0	6 7 . 3 0 0	1 . 3 2 3	3 0 . 7 1 0
1 6	2 7 5 . 3 8 6	8 4 . 8 3 0	2 6 5 . 2 0 0 0	6 7 4 . 2 0 0	1 . 5 5 2	4 1 . 7 0 0	1 . 0 3 8	3 3 . 6 3 0
1 7	2 9 1 . 3 0 1	8 6 . 2 3 0	2 2 1 . 6 0 0 0	6 2 0 . 2 0 0	1 . 7 0 5	6 1 . 2 0 0	1 . 3 1 3	3 4 . 1 8 0
1 8	2 4	6 9	2 1	5 6	1 .	4 7	1 .	2 7

	6 . 3 0 2	. 6 5 0	3 . 2 0 0	1 . 0 0 0	5 6 6	. 8 0 0	1 5 0	. 6 1 0
1 9	2 2 0 . 2 6 4	6 4 . 3 3 0	1 9 8 . 3 0 0	5 0 9 . 1 0 0	1 . 5 6 2	4 3 . 4 0 0	1 . 1 1 0	2 5 . 5 0 0
2 0	3 0 2 . 4 0 8	8 8 . 1 1 0	2 8 0 . 1 0 0	7 1 5 . 2 0 0	1 . 5 4 1	4 2 . 4 0 0	1 . 0 7 0	3 4 . 9 2 0
2 1	2 0 6 . 2 3 8	5 9 . 6 5 0	1 8 2 . 2 0 0	4 6 6 . 7 0 0	1 . 5 6 8	4 3 . 0 0 0	1 . 1 3 1	2 3 . 6 4 0
2 2	2 5 4 . 2 8 1	7 4 . 9 1 0	2 0 9 . 5 0 0	5 6 1 . 9 0 0	1 . 6 3 3	5 1 . 7 0 0	1 . 2 1 3	2 9 . 7 0 0
2 3	1 9 2 . 2 1 1	5 5 . 0 6 0	1 6 5 . 3 0 0	4 2 9 . 5 0 0	1 . 5 8 0	4 5 . 5 0 0	1 . 1 6 2	2 1 . 8 2 0
2 4	1 7 8 .	5 0 . 4	1 4 8 .	3 8 9 .	1 . 5 9	4 7 . 0	1 . 1 9	1 9 9

	1 8 5	3 0	8 0 0	7 0 0	2	0 0	7	9 0
2 5	2 8 5 . 2 5 2	7 6 . 8 4 0	2 0 6 . 1 0 0 0	5 7 7 . 7 0 0 0	1 . 6 6 8	6 1 . 6 0 0	1 . 3 8 3	3 0 . 4 6 0
2 6	2 3 4 . 2 9 1	6 8 . 9 2 0	2 1 5 . 2 0 0 0	5 4 6 . 2 0 0 0	1 . 5 5 3	4 1 . 5 0 0	1 . 0 8 8	2 7 . 3 2 0
2 7	2 8 4 . 2 6 7	7 9 . 7 0	2 0 1 . 6 0 0 0	5 8 0 . 0 0 0 0	1 . 7 2 1	6 8 . 4 0 0	1 . 4 0 9	3 1 . 6 2 0
2 8	2 7 3 . 7 1 4	7 8 . 1 2 0	2 0 1 . 7 0 0 0	5 6 0 . 4 0 0 0	1 . 7 0 1	5 9 . 5 0 0	1 . 3 5 6	3 0 . 9 7 0
2 9	3 1 5 . 3 6 5	9 7 . 7 0 0	2 5 4 . 9 0 0 0	7 0 2 . 1 0 0 0	1 . 6 9 2	5 7 . 5 0 0	1 . 2 3 7	3 8 . 7 3 0
3 0	2 8 9 . 3 2	9 1 . 0 7 0	2 2 3 . 9 0	6 2 8 . 3 0	1 . 7 4 8	6 2 . 0 0 0	1 . 2 9 2	3 6 . 1 0 0

	8		0	0				
3	3	8	2	6	1	6	1	3
1	1	4	1	1	.	9	.	3
	8	.	3	5	7	.	4	.
	.	6	.	.	2	1	9	5
	7	7	5	8	3	0	2	6
	1	0	0	0		0		0
	2		0	0				
3	2	7	2	5	1	5	1	3
2	7	8	0	6	.	9	.	0
	3	.	1	0	7	.	3	.
	.	1	.	.	0	5	5	9
	7	2	7	4	1	0	6	7
	1	0	0	0		0		0
	4		0	0				
3	2	7	1	5	1	5	1	2
3	3	3	8	2	.	8	.	9
	9	.	9	4	6	.	2	.
	.	2	.	.	9	3	6	0
	2	3	8	5	8	0	0	3
	6	0	0	0		0		0
	9		0	0				
3	2	6	1	5	1	5	1	2
4	3	5	8	0	.	4	.	5
	3	.	7	9	6	.	2	.
	.	5	.	.	1	8	4	9
	2	3	1	2	7	0	6	7
	6	0	0	0		0		0
	3		0	0				
3	1	5	1	4	1	4	1	2
5	9	7	6	3	.	7	.	2
	1	.	6	5	6	.	1	.
	.	0	.	.	0	1	5	6
	2	4	2	5	2	0	0	1
	2	0	0	0		0		0
	6		0	0				
3	2	8	2	5	1	5	1	3
6	6	2	2	9	.	2	.	2
	7	.	2	9	6	.	2	.
	.	8	.	.	6	9	0	8
	3	8	3	8	8	0	2	5
	2	0	0	0		0		0
	2		0	0				

Table A-III Regression parameters and quality of correlation when physicochemical parameters are used (pMIC_{ab})

M o d e l N o .	P a r a m e t e r u s e d	A_i=(1-6)	B	S e	R₂	R₂ A	F
1	M W	0.00 32(± 0.00 05)	0 . 4 8 5 7	0 . 0 8 1 0	0 . 5 5 4 5	0 . 5 4 1 4	4 2 . 3 1 2 0
2	M R	0.01 09(± 0.00 17)	0 . 5 0 4 1	0 . 0 8 4 0	0 . 5 2 0 0	0 . 5 0 5 9	3 6 . 8 3 3 0
3	P O L	0.02 75(± 0.00 45)	0 . 5 0 4 3	0 . 0 8 4 1	0 . 5 1 9 9	0 . 5 0 5 8	3 6 . 8 2 3 0
4	P C	0.00 14(± 0.00 03)	0 . 5 1 1	0 . 0 9 3	0 . 4 0 3	0 . 3 8 5	2 2 . 9 6

			8	7	2	6	9
5	I R	1.44 91(± 0.34 44)	- 1 . 0 6 5 9	0 . 0 9 8 4	0 . 3 4 2 4	0 . 3 2 3 0	1 7 . 7 0 0 0
6	S T	0.00 99(± 0.00 25)	0 . 7 7 5 9	0 . 0 9 9	0 . 3 2 1 3	0 . 3 0 1 4	1 6 . 0 9 7 0
7	D	0.68 35(± 0.18 96)	0 . 4 6 4 3	0 . 1 0 3 2	0 . 2 7 6 6	0 . 2 5 5 3	1 3 . 0 0 1 0
8	M V	0.00 28(± 0.00 09)	0 . 7 4 0 2	0 . 1 0 8 0	0 . 2 0 6 9	0 . 1 8 3 5	8 . 8 6 8 0
9	M R D	0.00 92(± 0.00 18) 0.36 38(± 0.15 93)	0 . 1 7 4 3	0 . 0 7 9 3	0 . 5 8 5 5	0 . 5 6 0 4	2 3 . 3 1 1 0
1 0	D P O L	0.36 38(± 0.15 93) 0.02 31(± 0.00	0 . 1 7 4 5	0 . 0 7 9 3	0 . 5 8 5 5	0 . 5 6 0 3	2 3 . 3 0 4 0

		46)					
1	M	0.00	-	0	0	0	2
1	W	27(±	0	.	.	.	2
	I	0.00	.	0	5	5	.
	R	06)	1	7	7	5	6
		0.49	8	9	8	3	6
		23(±	7	9	7	1	3
		0.35	5				0
		74)					
1	M	0.00	0	0	0	0	2
2	R	88(±	2
	S	0.00	3	0	5	5	.
	T	19)	9	8	7	5	4
		0.00	4	0	6	0	3
		48(±	8	2	2	5	1
		0.00					0
		23)					
1	S	0.00	0	0	0	0	2
3	T	477(.	.	.	.	2
	P	±0.0	3	0	5	5	.
	O	023)	9	8	7	5	4
	L	0.02	4	0	6	0	2
		22(±	9	2	1	4	4
		0.00					0
		49)					
1	M	-	0	0	0	0	2
4	V	0.00	2
	P	74(±	6	0	5	5	.
	C	0.00	1	8	7	4	0
		20)	2	0	2	6	5
		0.00	8	5	1	1	7
		39(±					0
		0.00					
		07)					
1	P	0.00	-	0	0	0	2
5	C	13(±	0	.	.	.	1
	D	0.00	.	0	5	5	.
		03)	0	8	7	4	8
		0.54	6	0	0	4	8
		17(±	6	7	2	1	9
		0.15	2				0
		13)					
1	M	0.00	0	0	0	0	2
6	W	28(±	1

	S T	0.00 06) 0.00 28(± 0.00 26)	4 4 4 7	0 8 0 8	5 6 9 7	5 4 3 6	. 8 4 8 0
1 7	M R M V	0.01 55(± 0.00 29) - 0.00 23(± 0.00 12)	0 .br/>6 4 1 7	0 .br/>0 8 0 9	0 .br/>5 6 8 7	0 .br/>5 4 2 6	2 1 .br/>7 5 7 0
1 8	M V P O L	- 0.00 23(± 0.00 12) 0.03 91(± 0.00 74)	0 .br/>6 4 1 8	0 .br/>0 8 0 9	0 .br/>5 6 8 6	0 .br/>5 4 2 4	2 1 .br/>7 4 5 0
1 9	M R D P O L	1.54 11(± 2.25 56) 0.37 05(± 0.16 09) - 3.86 47(± 5.69 00)	0 .br/>1 5 8 6	0 .br/>0 7 9 9	0 .br/>5 9 1 4	0 .br/>5 5 3 1	1 5 .br/>4 4 1
2 0	M W M R M V	0.00 19(± 0.00 15) 0.00 85(± 0.00	0 .br/>5 9 3 2	0 .br/>0 8 0 3	0 .br/>5 8 7 6	0 .br/>5 4 8 9	1 5 .br/>1 9 9

		64) - 0.00 19(± 0.00 13)						
2 1	M W M V P O L	0.00 19(± 0.00 15) - 0.00 19(± 0.00 13) 0.02 15(± 0.01 62)	0 . 5 9 3 2	0 . 0 8 0 3	0 . 5 8 7 5	0 . 5 4 8 9	1 5 . 1 9 5	
2 2	M R I R D	0.00 94(± 0.00 22) - 0.17 30(± 0.70 29) 0.43 48(± 0.33 06)	0 . 3 5 0 0	0 . 0 8 0 4	0 . 5 8 6 3	0 . 5 4 7 5	1 5 . 1 1 8	
2 3	I R D P O L	- 0.17 33(± 0.70 31) 0.43 49(± 0.33 06) 0.02 38(± 0.00	0 . 3 5 0 4	0 . 0 8 0 4	0 . 5 8 6 3	0 . 5 4 7 5	1 5 . 1 1 4	

		55)					
2	M	-	1	0	0	0	1
4	V	0.02	5
	P	49(±	4	0	5	5	.
	C	0.01	5	8	8	4	1
	S	69)	0	0	6	7	1
	T	0.01	5	4	2	4	0
		07(±					
		0.00					
		65)					
		-					
		0.01					
		79(±					
		0.01					
		71)					
2	M	0.00	0	0	0	0	1
5	W	02(±	5
	M	0.00	1	0	5	5	.
	R	21)	8	8	8	4	0
	D	0.00	8	0	5	6	8
		85(±	5	5	7	9	0
		0.00					0
		65)					
		0.34					
		49(±					
		0.23					
		48)					
2	M	0.00	0	0	0	0	1
6	W	02(±	5
	D	0.00	1	0	5	5	.
	P	21)	8	8	8	4	0
	O	0.34	8	0	5	6	7
	L	44(±	9	5	6	8	6
		0.23					0
		47)					
		0.02					
		13(±					
		0.01					
		64)					
2	M	0.00	0	0	0	0	1
7	R	86(±	5
	P	0.00	1	0	5	5	.
	C	78)	5	8	8	4	0
	D	8.77	6	0	5	6	7

		32(± 0.00 11) 0.37 51(± 0.21 46)	4	5	6	8	5 0
2 8	M R S T D	0.00 92(± 0.00 20) - 0.00 04(± 0.00 65) 0.39 00(± 0.45 73)	0 . 1 5 9 7	0 . 0 8 0 5	0 . 5 8 5 6	0 . 5 4 6 7	1 5 . 0 7 3 0
2 9	M R M V I R D	0.03 55(± 0.02 77) - 0.00 88(± 0.00 93) - 2.69 94(± 2.76 79) 0.45 22(± 0.33 16)	4 . 3 5 7 4	0 . 0 8 0 6	0 . 5 9 7 9	0 . 5 4 6 0	1 1 . 5 2 3 0
3 0	M V I R D P	- 0.00 88(± 0.00 94) -	4 . 3 3 1 9	0 . 0 8 0 6	0 . 5 9 7 6	0 . 5 4 5 7	1 1 . 5 1 1

	O L	2.68 37(± 2.77 16) 0.45 27(± 0.33 18) 0.08 92(± 0.07 004)					0
3 1	M W M R I R D	- 0.01 37(± 0.01 49) 0.05 64(± 0.05 12) - 4.63 23(± 4.90 57) 3.35 43(± 3.19 56)	4 . 0 6 0 6	0 . 0 8 0 6	0 . 5 9 7 3	0 . 5 4 5 3	1 1 . 4 9 4 0
3 2	M W I R D P O L	- 0.01 33(± 0.01 49) - 4.52 29(± 4.88 99) 3.28 18(± 3.18 44)	3 . 9 7 0 6	0 . 0 8 0 7	0 . 5 9 6 8	0 . 5 4 4 7	1 1 . 4 7 0 0

		0.13 93(± 0.12 86)					
3 3	M W M R I R P O L	0.00 17(± 0.00 16) 1.46 63(± 2.34 44) 0.54 39(± 0.37 09) - 3.69 06(± 5.91 27)	- 0 . 2 8 1 2	0 . 0 8 1 5	0 . 5 8 8 1	0 . 5 3 5 0	1 1 . 0 6 7 0
3 4	M W M V I R P O L	0.00 20(± 0.00 16) - 0.00 94(± 0.00 94) - 2.17 46(± 2.69 99) 0.07 64(± 0.07 01)	4 . 0 4 9 5	0 . 0 8 0 7	0 . 5 9 6 0	0 . 5 4 3 9	1 1 . 4 3 3 0
3 5	M R M V I	0.04 13(± 0.02 87) -	5 . 6 9 3	0 . 0 8 1	0 . 5 9 3	0 . 5 4 0	1 1 . 2 9

	R S T	0.01 09(± 0.00 97) - 3.38 92(± 3.03 12) 0.00 68(± 0.00 56)	9	0	1	6	8 0
3 6	M W M R M V P O L	0.00 17(± 0.00 16) 1.48 44(± 2.32 76) - 0.00 20(± 0.00 13) - 3.72 12(± 5.86 87)	0 . 5 9 3 6	0 . 0 8 1 1	0 . 5 9 2 9	0 . 5 4 0 4	1 1 . 2 8 6 0
3 7	M R P C I R S T	0.06 61(± 0.05 09) - 0.00 74(± 0.00 66) - 5.49 68(± 4.88	8 . 2 1 2 9	0 . 0 8 1 1	0 . 5 9 2 9	0 . 5 4 0 3	1 1 . 2 8 6 0

		89) 0.02 467(±0.0 181)						
3 8	M V I R S T P O L	- 0.01 09(± 0.00 97) - 3.37 26(± 3.03 62) 0.00 68(± 0.00 56) 0.10 38(± 0.07 25)	5 . 6 6 7 5	0 . 0 8 1 1	0 . 5 9 2 9	0 . 5 4 0 3	1 1 . 2 8 5 0	A - I V A c t u a l a

nd predicted value

S	A	Pr	R
.	c	ed	e
N	t	ict	s
o	u	ed	i
.	a	va	d
	l	lu	u
		e	a
	v	(p	l
	a	M	
	l	I	
	u	C_a	
	e	b)	
	(
	p		
	M		
	I		

C			
a			
b			
)			
1	1	1.	-
	.	26	0
	0	3	.
	8		1
	0		8
			3
2	1	1.	0
	.	24	.
	4	6	1
	0		5
	0		4
3	1	1.	-
	.	40	0
	3	9	.
	5		0
	0		5
			9
4	1	1.	-
	.	35	0
	2	1	.
	3		1
	0		2
			1
5	1	1.	0
	.	34	.
	5	7	1
	3		8
	0		3
6	1	1.	0
	.	50	.
	6	4	1
	1		0
	0		6
7	1	1.	0
	.	37	.
	4	0	0
	3		5
	0		9
8	1	1.	0
	.	28	.

	4	4	1
	0		1
	0		6
9	1	1.	-
	.	40	0
	3	3	.
	6		0
	0		4
			3
1	1	1.	0
0	.	14	.
	2	8	0
	2		7
	0		2
1	1	1.	-
1	.	31	0
	3	6	.
	1		0
	0		0
			6
1	1	1.	-
2	.	47	0
	3	2	.
	9		0
	0		8
			2
1	1	1.	-
3	.	40	0
	3	3	.
	6		0
	0		4
			3
1	1	1.	-
4	.	45	0
	2	8	.
	8		1
	0		7
			8
1	1	1.	-
5	.	31	0
	3	6	.
	1		0
	0		0
			6

1	1	1.	-
6	.	45	0
	2	8	.
	4		0
	0		6
			9
1	1	1.	0
7	.	45	.
	6	6	2
	7		1
	0		4
1	1	1.	-
8	.	24	0
	1	2	.
	9		5
	0		2
			2
1	1	1.	-
9	.	17	0
	1	7	.
	5		0
	0		2
			7
2	1	1.	0
0	.	33	.
	3	9	0
	8		4
	0		1
2	1	1.	-
1	.	14	0
	1	7	.
	2		0
	0		2
			6
2	1	1.	-
2	.	30	0
	2	9	.
	1		0
	0		9
			9
2	1	1.	0
3	.	11	.
	1	4	0
	9		7

	0		6
2	1	1.	0
4	.	07	.
	1	9	0
	5		7
	0		1
2	1	1.	-
5	.	39	0
	3	1	.
	6		0
	0		3
			1
2	1	1.	-
6	.	20	0
	1	6	.
	7		0
	0		3
			6
2	1	1.	-
7	.	40	0
	2	3	.
	6		1
	0		4
			4
2	1	1.	0
8	.	37	.
	4	4	0
	4		6
	0		6
2	1	1.	0
9	.	57	.
	6	0	0
	0		2
	0		9
3	1	1.	-
0	.	48	0
	4	2	.
	6		0
	0		2
			2
3	1	1.	0
1	.	50	.
	5	4	0
	1		0

	0		6
3	1	1.	0
2	.	37	.
	5	4	1
	4		6
	0		6
3	1	1.	0
3	.	27	.
	3	0	1
	8		1
	0		0
3	1	1.	-
4	.	23	0
	1	2	.
	7		0
	0		6
			2
3	0	1.	-
5	.	12	0
	9		.
	8		1
	0		3
			2
3	1	1.	-
6	.	38	0
	3	0	.
	3		0
	0		5
			0

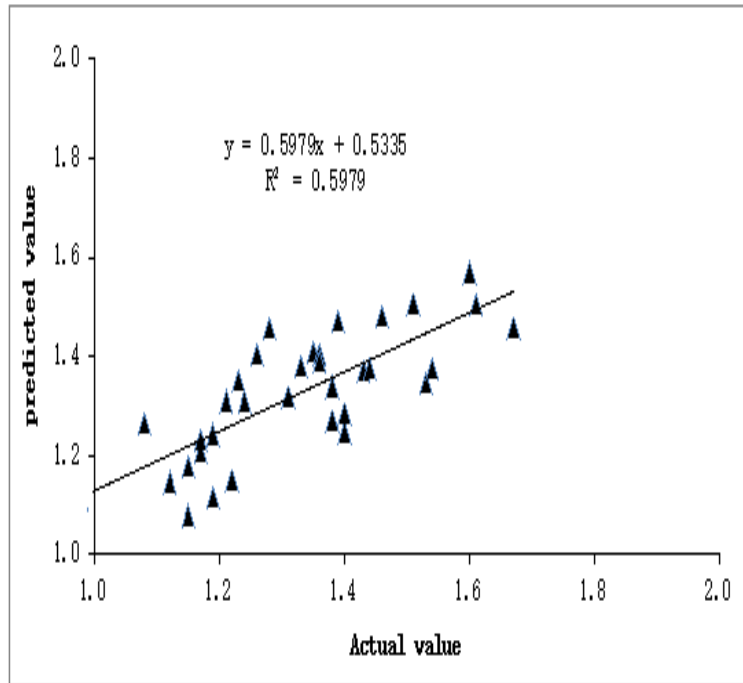


Fig. (a) correlation between actual and predicted pMIC_{ab} values.

Table A-V Cross- validated parameters for the best obtained models

M o d e l N o .	P a r a m e t e r s u s e d	P R E S S / S S Y	R ² c v	S p r e s s	P S E
1	M W	0 . 8 0 3 6	0 . 1 9 6 4	0 . 0 1 8 4	0 . 0 1 7 4
9	M R D	0 . 7 0 7 8	0 . 2 9 2 2	0 . 0 1 8 3	0 . 0 1 6 8
1 9	M R D P O L	0 . 6 9 0 8	0 . 3 0 9 2	0 . 0 1 8 7	0 . 0 1 6 7
3 0	M V I R D P O L	0 . 6 7 3 3	0 . 3 2 6 7	0 . 0 1 9 2	0 . 0 1 6 5

B} Modeling pMIC_{am} using physicochemical parameter

A close look of tableB-I reveals that

1) Out of Eight mono-parametric model,MW shows the highest regression value for the best model.

- 2) Out of ten bi-parametric model, PC and D together shows the highest regression value for the best model.
- 3) Out of ten tri-parametric model, MW, MR and POL together shows the highest regression value for the best model.
- 4) Out of ten tetra-parametric model, MR, PC, D and POL together shows the highest regression value for the best model.

Mono-Parametric model

$$pMIC_{am} = 0.0027(\pm 0.0004)MW + 0.5936 \quad (B-1)$$

$$N=37, R^2=0.5511, R^2A=0.5379, Se=0.0696, F=41.7360$$

When PC and D were taken together a bi-Parametric model has been obtained with improved statistics here R^2 comes out to be 0.5581.

Bi-Parametric model

$$pMIC_{am} = 0.0011(\pm 0.0002)PC + 0.4063 (\pm 0.1281)D + 0.1628$$

(B-2)

$$N=37, R^2 = 0.5581, R^2A = 0.5313, Se=0.0701, F=20.8410$$

A tri-Parametric model has been obtained when MW, MR and POL were taken together. In this model the R^2 shows significant improvement.

Tri-Parametric model

$$pMIC_{am} = 0.0028(\pm 0.0013)MW + 1.9426(\pm 1.9498)MR$$

$$-4.9013(\pm 4.9174)POL + 0.5864 \quad (B-3)$$

$$N=37, R^2=0.5649, R^2A=0.5242, Se=0.0706, F=13.8510$$

A tetra-parametric model has been obtained when MR, PC, D and POL were taken together. In this model the R^2 shows significant improvement.

Tetra-Parametric model

However, very small improvement is observed in a tetra-parametric model when MR, PC, D and POL have been taken as correlating parameter. This model has been found to be excellent for modeling activity of the compounds of the present study.

$$pMIC_{am} = 2.2019(\pm 1.9775)MR + 0.0011(\pm 0.0009)PC + 0.4257(\pm 0.1846)D + 5.5558(\pm 4.9858)POL +$$

$$0.1328 \quad (B-4) \quad N=37, R^2=0.5759, R^2A=0.5212, Se=0.0709, \quad F=10.5250.$$

Validation of model

The model has been validated by plotting a graph actual and predicted value of $pMIC_{am}$ activity as recorded in Table B-II obtained from tetra-parametric model.

Cross- validated parameters

In this we observed the parameter with the high regression value which will obtained the best result.

We have estimated pMIC_{am} values using Model-29. The predictive power of best Model has been obtained by plotting graph between actual and predicted pMIC_{am} values demonstrated in Fig. (b).

This clearly indicates that this is best model for estimating predicting pMIC_{am} values of the compounds in the present study.

Table B-I Regression parameters and quality of correlation when physicochemical parameters are used (pMIC_{am})

Model No.	parameter used	A _i =(1-6)	B	Se	R ₂	R ₂ A	F
1	MW	0.0027(±0.0004)	0 . 5 9 3 6	0 . 0 6 9 6	0 . 5 5 1 1	0 . 5 3 7 9	4 1 . 7 3 6 0
2	MR	0.0087(±0.0016)	0 . 6 3 3 2	0 . 0 7 4 9	0 . 4 8 0 9	0 . 4 6 5 6	3 1 . 4 9 5 0
3	POL	0.0220(±0.0039)	0 . 6	0 . 0	0 . 4	0 . 4	3 1 .

			3	7	8	6	4
			3	4	0	5	7
			3	9	7	5	6
							0
4	P C	0.001 2(±0. 0002)	0	0	0	0	2
			4
			5	0	4	4	.
			9	7	2	0	9
			6	8	3	6	7
			3	9	5	5	6
							0
5	S T	0.007 7(±0. 0021)	0	0	0	0	1
			3
			8	0	2	2	.
			6	8	8	6	2
			3	8	1	0	9
			6	1	1	0	7
							0
6	I R	1.033 5±(0. 3073)	-	0	0	0	1
			0	.	.	.	1
			.	0	2	2	.
			4	9	4	2	3
			1	0	9	7	0
			2	0	6	5	8
			5				0
7	M V	0.002 5(±0. 0007)	0	0	0	0	1
			0
			7	0	2	2	.
			6	9	3	1	6
			7	0	8	6	5
			7	7	7	3	8
							0
8	D	0.529 9(±0. 1625)	0	0	0	0	1
			0
			6	0	2	2	.
			2	9	3	1	6
			5	0	8	5	3
			3	7	3	9	6
							0
9	P C D	0.001 1(±0. 0002) 0.406 3(±0. 1281)	0	0	0	0	2
			0
			1	0	5	5	.
			6	7	5	3	8
			2	0	8	1	4
			8	1	1	3	1
							0
1 0	M W S T	0.002 4(±0. 0005) 0.001	0	0	0	0	2
			0
			5	0	5	2	.
			7	7	5	3	7

		5(±0.0022)	19	02	72	03	61
11	MW MV	0.0029(±0.0006)	062	0075	0053	0026	2048
		4(±0.0008)	2	4	9	8	50
12	MW D	0.0025(±0.0003)	054	0072	0053	0026	2049
		0.0694(±0.01582)	424	705	537	266	4690
13	MW IR	0.0025(±0.0005)	041	0079	0053	0026	2044
		0.1273(±0.03074)	95	0055	34	63	450
14	MW PC	0.0029(±0.0009)	060	0079	0052	0024	2033
		0.0001(±0.0005)	4	6	0	9	30
15	MW POL	0.0029(±0.0013)	059	0077	0051	0024	2085
		0.0018(±0.0111)	2	6	4	3	50
16	MW MR	0.0029(±0.0013)	059	0077	0051	0024	2084
		0.007(±0.0044)	72	0066	14	42	840
17	MV D	0.0029(±0.0006)	060	0077	0053	0026	2042
		0.6119(±0.1278)	85	0077	007	35	226

			8				0
1	M	-	0	0	0	0	2
8	V	0.005	0
	P	4(±0.	6	0	5	5	.
	C	0018)	6	7	5	2	1
		0.003	9	0	0	3	9
		1(±0.	4	7	3	1	2
		0006)					0
1	M	0.002	0	0	0	0	1
9	W	8(±0.	3
	M	0013)	5	0	5	5	.
	R	1.942	8	7	6	2	8
	P	6(±1.	6	0	4	4	5
	O	9498)	4	6	9	2	1
	L	-					0
		4.901					
		3(±4.					
		9174)					
2	M	0.001	0	0	0	0	1
0	W	6(±0.	3
	M	0019)	6	0	5	5	.
	V	-	4	7	6	1	6
	P	0.002	1	1	0	9	0
	C	8(±0.	2	0	6	4	8
		0035)					0
		0.001					
		4(±0.					
		0020)					
2	M	0.002	0	0	0	0	1
1	W	5(±0.	3
	S	0005)	6	0	5	5	.
	T	0.003	5	7	5	1	5
	D	4(±0.	8	1	9	8	4
		0053)	3	1	5	2	6
		-					0
		0.156					
		1(±0.					
		3827)					
2	M	0.001	0	0	0	0	1
2	W	8(±0.	3
	P	0018)	5	0	5	5	.
	C	0.000	2	7	5	1	5
	S	3(±0.	1	1	9	7	3
	T	0008)	4	1	2	9	1
		0.002					0
		5(±0.					
		0034)					
2	M	0.002	0	0	0	0	1
3	W	5(±0.	3
	I	0006)	8	0	5	5	.

	R S T	- 0.251 1(±0. 6624) 0.003 0(±0. 0047)	9 1 9	7 1 1	5 9 2	1 7 8	5 2 9 0
2 4	P C D P O L	0.001 3(±0. 0009) 0.438 7(±0. 1849) - 0.004 2(±0. 0170)	0 . 1 1 9	0 . 0 7 1 1	0 . 5 5 9 0	0 . 5 1 7 6	1 3 . 5 1 9 0
2 5	P C I R D	0.001 1(±0. 0002) - 0.134 8(±0. 5492) 0.466 9(±0. 2791)	0 . 2 9 8 8	0 . 0 7 1 1	0 . 5 5 9 0	0 . 5 1 7 6	1 3 . 5 1 8 0
2 6	M R P C D	- 0.001 6(±0. 0068) 0.001 3(±0. 0009) 0.438 2(±0. 1849)	0 . 1 2 0 2	0 . 0 7 1 1	0 . 5 5 8 9	0 . 5 1 7 6	1 3 . 5 1 7 0
2 7	M V P C D	- 0.001 2(±0. 0055) 0.001 6(±0. 0020) 0.031 8(±0. 4036)	0 . 2 7 4 3	0 . 0 7 1 1	0 . 5 5 8 9	0 . 5 1 7 5	1 3 . 5 1 3 0
2 8	M W M	0.001 9(±0. 0018)	0 . 4	0 . 0	0 . 5	0 . 5	1 3 .

	V S T	0.000 6(±0. 0019) 0.002 9(±0. 0049)	9 9 2	7 1 1	5 8 7	1 7 3	5 0 4 0
2 9	M R P C D P O L	2.201 9(±1. 9775) 0.001 1(±0. 0009) 0.425 7(±0. 1846) - 5.555 8(±4. 9858)	0 . 1 3 2 8	0 . 0 7 0 9	0 . 5 7 5 9	0 . 5 2 1 2	1 0 . 5 2 5
3 0	M W M R S T P O L	0.002 0(±0. 0015) 2.203 3(±1. 9854) 0.001 9(±0. 0024) - 5.555 0(±5. 0065)	0 . 5 4 8 6	0 . 0 7 1 0	0 . 5 7 4 2	0 . 5 1 9 2	1 0 . 4 5 1 0
3 1	M R I R D P O L	2.220 3(±1. 9907) - 0.653 8(±0. 6166) 0.547 3(±0. 2876) - 5.579 7(±5. 0221)	1 . 0 2 9 9	0 . 0 7 1 2	0 . 5 7 1 9	0 . 5 1 6 7	1 0 . 3 5 5 0
3 2	M R M V	2.275 1(±1. 9874) -	0 . 6 6	0 . 0 7	0 . 5 7	0 . 5 1	1 0 . 3

	P C P O L	0.006(±0.00 28) 0.003 6(±0. 0019) - 5.743 9(±5. 0109)	2 2	1 3	1 0	5 6	1 4 0
3 3	M W M R D P O L	0.001 9(±0. 0019) 2.181 1(±2. 0057) 0.128 5(±0. 2067) - 5.497 2(±5. 0569)	0 . 4 7 9 2	0 . 0 7 1 3	0 . 5 7 0 3	0 . 5 1 4 9	1 0 . 2 8 6 0
3 4	M W M R M V P O L	0.002 5(±0. 0013) 2.150 5(±1. 9978) - 0.000 7(±0. 0011) - 5.420 2(±5. 0371)	0 . 6 2 8 1	0 . 0 7 1 3	0 . 5 7 0 2	0 . 5 1 4 7	1 0 . 2 8 1 0
3 5	M R M V D P O L	2.277 9(±1. 9902) 0.002 0(±0. 0021) 0.515 5(±0. 2770) - 5.740 4(±5. 0185)	0 . 0 3 1 2	0 . 0 7 1 4	0 . 5 6 9 8	0 . 5 1 4 3	1 0 . 2 6 5 0

3 6	M W M R I R P O L	0.002 5(±0. 0014) 2.150 1(±2. 0018) 0.185 3(±0. 3167) - 5.424 2(±5. 0485)	0 . 3 3 1 1	0 . 0 7 1 4	0 . 5 6 9 7	0 . 5 1 4 2	1 0 . 2 6 0 0
3 7	M R I R S T P O L	2.289 3(±1. 9972) - 0.796 0(±0. 7112) 0.008 53(±0 .0047) - 5.755 2(±5. 0386)	1 . 5 2 7 5	0 . 0 7 1 5	0 . 5 6 7 7	0 . 5 1 1 9	1 0 . 7 1 8 0
3 8 .	M W M R P C P O L	0.002 7(±0. 0013) 2.067 9(±2. 0042) - 0.000 3(±0. 0007) - 5.212 9(±5. 0527)	0 . 6 0 9 9	0 . 0 7 1 6	0 . 5 6 6 9	0 . 5 1 1 0	1 0 . 1 4 5 0

Table B-II Actual and predicted value

S . N o .	A c t u a l v a l u e (P M I C a m)	Pr ed ict ed va lu e (p M I C am)	R e s i d u a l
1	1 . 1 6 0	1. 21 4	- 0 . 0 5 4
2	1 . 3 6 0	1. 26 2	0 . 0 9 8
3	1 . 3 5 0	1. 35 7	- 0 . 0 0 7
4	1 . 2 7 0	1. 29 5	- 0 . 0 2 5
5	1	1.	0

	.	32	.
	3	5	0
	9		6
	0		5
6	1	1.	0
	.	45	.
	5	9	0
	3		7
	0		1
7	1	1.	-
	.	33	0
	3	9	.
	3		0
	0		0
			9
8	1	1.	0
	.	27	.
	3	6	0
	6		8
	0		4
9	1	1.	0
	.	37	.
	4	1	0
	2		4
	0		9
1	1	1.	0
0	.	13	.
	1	7	0
	6		2
	0		3
1	1	1.	0
1	.	30	.
	3	6	0
	1		0
	0		4
1	1	1.	-
2	.	39	0
	3	3	.
	3		0
	0		6
			3
1	1	1.	-
3	.	37	0
	3	1	.
	0		0
	0		7
			1
1	1	1.	-

4	.	42	0
	3	1	.
	2		1
	0		0
			1
1	1	1.	-
5	.	29	0
	2	2	.
	5		0
	0		4
			2
1	1	1.	-
6	.	29	0
	2	6	.
	2		0
	0		7
			6
1	1	1.	0
7	.	37	.
	7	8	3
	3		5
	0		2
1	1	1.	-
8	.	23	0
	1	4	.
	7		0
	0		6
			4
1	1	1.	-
9	.	16	0
	1	6	.
	3		0
	0		3
			6
2	1	1.	0
0	.	41	.
	4	2	0
	4		2
	0		8
2	1	1.	-
1	.	15	0
	1	6	.
	0		0
	0		5
			6
2	1	1.	-
2	.	23	0
	1	3	.

	9		0
	0		4
			3
2	1	1.	0
3	.	13	.
	1	1	0
	9		5
	0		9
2	1	1.	0
4	.	07	.
	1	2	0
	5		7
	0		8
2	1	1.	-
5	.	35	0
	3	1	.
	0		0
	0		5
			1
2	1	1.	0
6	.	19	.
	2	5	0
	1		1
	0		5
2	1	1.	-
7	.	37	0
	3	1	.
	0		0
	0		7
			1
2	1	1.	0
8	.	30	.
	3	4	0
	4		3
	0		6
2	1	1.	0
9	.	41	.
	4	7	0
	6		4
	0		3
3	1	1.	-
0	.	36	0
	2	9	.
	4		1
	0		2
			9
3	1	1.	-
1	.	45	0

	4	9	.
	1		0
	0		4
			9
3	1	1.	0
2	.	30	.
	4	4	0
	0		9
	0		6
3	1	1.	0
3	.	23	.
	2	3	0
	8		4
	0		7
3	1	1.	-
4	.	25	0
	1	6	.
	5		1
	0		0
			6
3	1	1.	-
5	.	10	0
	0	3	.
	6		0
	0		4
			3
3	1	1.	-
6	.	32	0
	2	0	.
	7		0
	0		5
			0

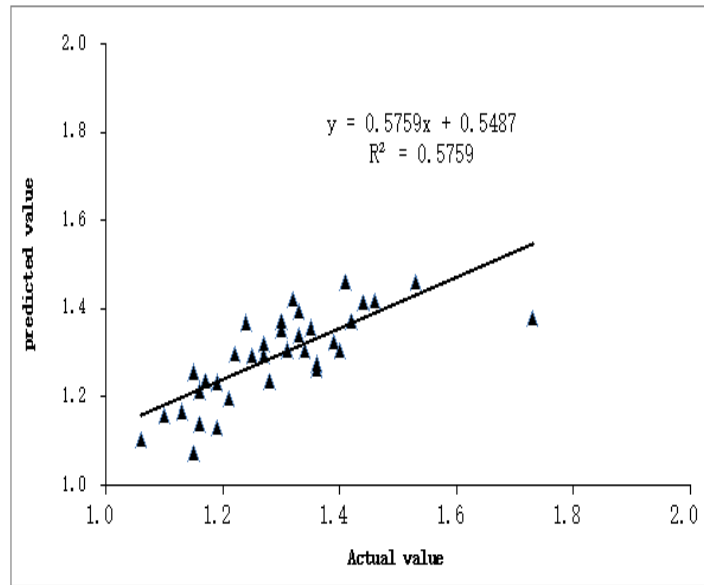


Fig. (b) correlation between actual and predicted pMIC_{am} values.

Table B-III Cross- validated parameters for the best obtained models

M o d e l N o .	P a r a m e t e r s u s e d	P R E S S / S S Y	R ² c v	S p r e s s	P S E
1	M W	0 . 8 1 4 6	0 . 1 8 5 4	0 . 0 1 5 4	0 . 0 1 4 6
9	P C D	0 . 7 9 1 7	0 . 2 0 8 3	0 . 0 1 5 8	0 . 0 1 4 5
1 9	M W M R P O L	0 . 7 7 0 1	0 . 2 2 9 9	0 . 0 1 6 2	0 . 0 1 4 4
3 0	M W M R S T P O L	0 . 0 7 4 2	0 . 9 2 5 8	0 . 0 1 6 5	0 . 0 1 4 2

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